## Hydrogen safety in chlor-alkali

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## Introduction

- Production of chlorine and hydrogen are coupled
  - $2NaCl + 2H_2O \longrightarrow Cl_2 + H_2 + 2NaOH$
- Unless you use the ODC process –  $2NaCl + H_2O + \frac{1}{2}O_2 \longrightarrow Cl_2 + 2NaOH$
- H<sub>2</sub> can be more or less in every part of the chlor-alkali installation
- The electrolyser is not the only source of the H<sub>2</sub>



### Introduction

- Other H<sub>2</sub> sources in the chlor-alkali installation
  - Acid (e.g. HCl,  $H_2SO_4$ ) in contact with metals generates  $H_2$

$$H_{2}SO_{4 (aq)} + Fe_{(s)} \longrightarrow H_{2(g)} + Fe^{2+}_{(aq)} + SO_{4}^{2-}_{(aq)}$$
  
2HCl<sub>(aq)</sub> + Fe<sub>(s)</sub> \longrightarrow H\_{2(g)} + Fe^{2+}\_{(aq)} + 2Cl^{-}\_{(aq)}



oroSur

Video: Aluminum foil + HCl solution

- Melting FeCl<sub>3</sub>.xaq can create and acid environment and the acid can react with the metal and form H<sub>2</sub>

FeCl<sub>3</sub> +  $3H_2O$  2HCl + Fe Fe(OH)<sub>3</sub> + 3HCl (0.1 M solution pH = 2) FeCl<sub>2</sub> +  $H_2$ 

## **Explosion limits**

- Explosion limits and the effect of temperature<sup>1)</sup>
  - The effect of pressure is limited<sup>1)</sup> for chlorine the lower explosion limit become 2.5 3 vol% at 13.5 bar(a)

Temperature in °C	H <sub>2</sub> – Air (vol% H <sub>2</sub> )	$H_2 - O_2$ (vol% $H_2$ )	$H_2 - Cl_2$ (vol% $H_2$ )
Minus 60	4.0 - 69	4.0 - 96	5.0 - 90.0
Minus 40	4.0 - 71	4.0 - 96	4.0 - 90.5
Minus 20	4.0 - 72	4.0 - 96	4.0 - 91.5
0	4.0 - 73	4.0 - 96	3.5 - 92.0
20 – 25	4.0 - 75	4.0 - 96	3.0 - 92.5
50	3.7 - 76	4.0 - 96	3.0 - 93.0
100	3.0 - 80	4.0 - 97	3.0 - 93.0

- Ignition energy is very low 10<sup>-7</sup> J
- Auto ignition temperature H<sub>2</sub> Cl<sub>2</sub> mixtures is 207 °C (for H<sub>2</sub>-air it is 400 °C)



# **Explosion limits in the system Cl\_2 - H\_2 - O\_2**

- Explosion limits
  - No reaction
  - Mild explosion 2 times initial pressure
  - Strong explosion 6 times initial pressure
    - Detonations 50 times initial pressure



## **Explosion limits**

• Effects of Inert gases is limited



#### **Electrolysers**

- Normal operating conditions:
  - Cl<sub>2</sub>: 97.0 99.9 vol% (dry basis)
  - O<sub>2</sub>: 0.1 2.5 vol% (dry basis)
  - H<sub>2</sub>: 0.0 0.5 vol% (dry basis)
  - $H_2O$ : 40.0 60.0 vol% (highly influenced by operating temp.)
- Water reduces the concentrations and consequently, the risk of having an explosive mixture
- <u>Caution</u>: water concentration decreases dramatically during cooling and drying of the Cl2-gas, So do not count on the dilution effect of water
- <u>Main risk</u>: when hydrogen levels increase above normal; e.g. membrane leakages



#### Electrolysers

#### Preventive measures

- Purge with nitrogen when taking electrolyzers out of operation
- Measure hydrogen in chlorine gas (early detection/early warning)
- Have a cell voltage monitoring system (early detection/waring for leaking membranes
- Be aware that condensate from hydrogen system is saturated with hydrogen, have sufficient dilution air or purge collection systems continuously with nitrogen
- The cell room has normally not an explosion proof (ATEX) design; but take care that hydrogen cannot accumulate in the top of the roof



- During the cooling and drying the water will be removed but the hydrogen concentration (on dry basis) doesn't change. Normal operating conditions:
  - Cl<sub>2</sub>: 97.0 99.9 vol% (dry basis)
  - O<sub>2</sub>: 0.1 2.5 vol% (dry basis)
  - H<sub>2</sub>: 0.0 0.5 vol% (dry basis)
- <u>Main risk</u>: when hydrogen levels increase above normal; e.g. membrane leakages the risk of an explosive mixture increase
- During the chlorine liquefaction the H<sub>2</sub> and O<sub>2</sub> concentration starts to increase; With an increasing risk of getting an explosive mixture.
  - Especially when hydrogen concentration increases in gas from electrolyzers e.g. due to membrane damages



- Assume the following conditions:
  - Cl<sub>2</sub>: 99.35 vol%
  - O<sub>2</sub>: 0.50 vol%
  - H<sub>2</sub>: 0.15 vol%
  - 8 bar(abs) and 90 °C
- Condensation starts at 25.8 °C
  - In the graph, H<sub>2</sub> concentration is presented as a function of the condensation temperature



- At temperatures < 21 °C the gas mixture is explosive
  - Liquefaction efficiency 96%
- At temperatures < -40 °C the gas mixture is in the detonation zone

![](_page_11_Figure_5.jpeg)

#### **Chlorine cooling and liquefaction**

#### Preventive/control measures

- Measure hydrogen in chlorine gas at electrolysers (early detection/early warning)
- Have a cell voltage monitoring system (early detection/waring for leaking membranes)
- Measure H<sub>2</sub> concentration after each condensation step and use this to control temperature of the condensation and/or nitrogen intake

#### Safe guards:

- Have a safety function at high H<sub>2</sub> concentration:
  - Stop production and purge with N<sub>2</sub>
- Make condensation system explosion proof

![](_page_12_Figure_10.jpeg)

- What happens if (suddenly) the H<sub>2</sub> level in the gas from the electrolyser increases?
- Take the previous example; assume H<sub>2</sub> in cell gas increases from 0.15% to 0.3%

	99.35 vol%			Cl <sub>2</sub> :	99.20 vol%	
	0.50 vol%			• O <sub>2</sub> :	0.50 vol%	
_	0.15 vol%			H <sub>2</sub> :	0.30 vol%	
	os) & condensation at 21 °C	2		► 8 bar(a	bs) & condensation at 2	21 °C
concentration after condenser 2.9 vol%		H <sub>2</sub> cond	H <sub>2</sub> concentration after condenser <b>4.81 vol%</b>			
	99.20 vol%	ocre	ase condens			Add .5vol% N2/dry-air
	0.50 vol%				99.20 vol%	
	0.50 vol%			O <sub>2</sub> :	99.20 vol% 0.50 vol%	
	0.50 vol% 0.30 vol%			O <sub>2</sub> : H <sub>2</sub> :	99.20 vol% 0.50 vol% 0.30 vol%	
(at	0.50 vol% 0.30 vol% )s) & condensation at <b>23 °C</b>			O <sub>2</sub> : H <sub>2</sub> : 8 bar(a	99.20 vol% 0.50 vol% 0.30 vol% bs) & condensation at	21 °C
r(at	0.50 vol% 0.30 vol% os) & condensation at <b>23 °C</b> entration after condenser <b>2</b>	2.94 vol%		$O_2$ : $H_2$ : 8 bar(a $H_2$ cone	99.20 vol% 0.50 vol% 0.30 vol% bs) & condensation at centration after conde	21 °C nser <b>2.96 vol%</b>

**Chlorine cooling and liquefaction** 

- Why does the decrease of electrolyser load not help?
- The upset is probably caused by an increase in "pinholes" in membranes
- Increased holes means increased flow of hydrogen to chlorine
- Lower production doesn't decrease the H<sub>2</sub> through the membrane, it only decreases the chlorine production and (slightly) the H<sub>2</sub> production of the leakage current
  - Effect =  $H_2$  concentration in chlorine increases even further

#### -Wrong measure

![](_page_14_Picture_8.jpeg)

#### **Chlorine absorption**

- In Cl<sub>2</sub> absorption all kind of gasses containing Cl<sub>2</sub> are treated
- These gases will also contain H<sub>2</sub>
- In the absorption, Cl<sub>2</sub> will react but H<sub>2</sub> and O<sub>2</sub> remain
- Risk of getting explosive mixtures
- Measure:
  - Always ensure sufficient air or nitrogen flow to absorption to ensure under all conditions sufficient low H<sub>2</sub> concentrations

![](_page_15_Picture_8.jpeg)

Catholyte circulation, caustic evaporation, caustic storage

- The caustic from the electrolysers is saturated with H<sub>2</sub>
- The caustic circulation tank normally connected with H<sub>2</sub> system,
  - So only gas bubbles will be released, caustic will remain saturated
- If caustic is further concentrated in an evaporation the hydrogen will escape together with the water vapor
  - Check if the vent system/vacuum system of the caustic evaporation can contain explosive mixtures
- For the storage (mainly for caustic from electrolysers) ensure that hydrogen cannot accumulate in the top of storge tanks
  - E.g. have a small N<sub>2</sub> purge on the storage tanks

![](_page_16_Picture_9.jpeg)

#### Hydrogen cooling

- The hydrogen cell gas will normally be cooled
  - The condensate will be saturated with H<sub>2</sub>
  - Be aware: spaces above open drains and trenches might be flammable
    - Important awareness for work activities around these area's as the environment may eb explosive
- Hydrogen vent stack
  - Ensure that there is no possibility for ingress of air into the hydrogen system
    - e.g. a continuous positive flow of N<sub>2</sub> and/or a water seal

![](_page_17_Picture_9.jpeg)

#### **HCl production and Acid tanks**

- In the HCl production (from  $Cl_2 + H_2$ ) normally and excess  $H_2$  is used.
  - Ensure the vent gas outlet is at a safe place
  - The vent gas stream can be flammable and/or explosive
  - The produced HCl solution is saturated with H<sub>2</sub>
  - Ensure adequate venting and blanketing practices
- Hydrochloric acid storage tanks
  - H<sub>2</sub> can come from the saturated HCl solution form the HCl production
  - H<sub>2</sub> generation due damaged protective layer (of metal tanks)
  - Ensure adequate venting and blanketing practices

![](_page_18_Picture_11.jpeg)

### Conclusions

- $\succ$  Cl<sub>2</sub> will always contain a small amount of H<sub>2</sub>
- Dangerous situations can occur everywhere in the process
- It is advised to measure hydrogen:
  - After the electrolysers
  - After the condensation or in between the different condensation steps
- Have sufficient control in the condensation when H<sub>2</sub> levels increase
  - Adding N<sub>2</sub> or (dry) Air
  - Increase condensation temperature
- Always add sufficient amounts of fresh air to the absorption to avoid explosive/detonative mixtures

![](_page_19_Picture_10.jpeg)

### Conclusions

- $\succ$  H<sub>2</sub> can not only cause problems in the chlorine system
- Be aware of hydrogen releases and thus potential risks of fire/explosions in
  - Hydrogen condensate system
  - Caustic evaporation
  - Caustic storage
  - Hydrochloric acid production
  - Acid storage tanks

➢ Install sufficient measure to avoid accumulation of H₂

![](_page_20_Picture_9.jpeg)

### Thank You Ton Manders (tma@cefic.be)

![](_page_21_Picture_1.jpeg)